# Specification Sheet: Alloy 800H/800HT (UNS N08810, UNS N08811) W. Nr. 1.4958, 1.4959

# Nickel-Iron-Chromium Alloys Designed to Resist Oxidation and Carburization with Higher Creep and Stress Rupture Properties than Alloy 800 (UNS N08800)

Alloys 800H (UNS N08810) and 800HT (UNS N08811) are dualcertifiable Nickel-Iron-Chromium materials that resist oxidation, carburization and other high temperature corrosion. The chemical composition of the two alloys are identical to Alloy 800 (UNS N08800), with the exception of the higher level of carbon present in both grades -(0.05-0.10%) in alloy 800H, and (0.06-0.10%) in alloy 800HT. Alloy 800HT also has an addition of up 1.0 % aluminum and titanium. In addition to the chemistry restrictions, both alloys receive a high temperature annealing treatment that produces an average grain size of ASTM 5 or coarser. The restricted chemical compositions, combined with the high temperature anneal, assure these materials have greater creep and rupture strength when compared to Alloy 800.

Alloy 800H has good creeprupture properties at temperatures above 1100°F (600°C). It remains ductile during long term use at temperatures below 1290°F (700°C) due to a maximum titanium and aluminum content of 0.7%. Alloy 800 with a standard anneal is recommended for service below 1100°F (600°C). Alloy 800H resists reducing, oxidizing and nitriding atmospheres, as well as, atmospheres that alternate between reducing and oxidizing. The alloy remains stable in long term high temperature service.

Alloy 800HT has excellent creep strength at temperatures above 1290°F (700°C). If the application involves frequent temperature excursions under 1290°F (700°C) or parts of are permanently exposed to a temperature below 1290°F (700°C), Alloy 800H should be utilized. The high temperature resistance of Alloy 800HT is comparable to Alloy 800H. It also remains stable in long term high temperature service.

Alloys 800H and 800AT are easily welded and processed by standard shop fabrication practices.

### **Applications**

- Chemical and Petrochemical Processing process equipment for the production of ethylene, ethylene dichloride, acetic anhydride, ketene, nitric acid and oxy-alcohol
- Petroleum Refining steam/hydrocarbon reformers and hydrodealkylation units
- Power Generation steam super-heaters and high temperature heat exchangers in gas-cooled nuclear reactors, heat exchangers and piping systems in coal-fired power plants
- Thermal Processing Fixtures radiant tubes, muffles, retorts and fixtures for heat-treating furnaces

## **Standards**

ASTM	B 409			
ASME	SB 409			
AMS	5871			

# **Chemical Analysis**

Weight % (all values are maximum unless a range is otherwise indicated)

Element	800H	800H 800HT	
Nickel	30.0 min35.0 max.	30.0 min35.0 max.	
Chromium	19.0 min23.0 max.	19.0 min23.0 max.	
Iron	39.5	39.5	
Carbon	0.05 min0.10 max.	0.06 min0.10 max.	
Manganese	1.50	1.50	
Phosphorus	0.045	0.045	
Sulfur	0.015 0.015		
Silicon	Silicon 1.0		
Aluminum	uminum 0.15 min.–0.60 max. 0.25 min.–0.60 ma		
Titanium	um 0.15 min0.60 max. 0.25 min0.60 max.		
Aluminum & Titanium	0.30 min1.20 max.	0.85 min1.20 max.	

# **Physical Properties**

Density 0.287 lbs/in<sup>3</sup> 7.94 g/cm<sup>3</sup> Specific Heat 0.11 BTU/lb-°F (32–212°F) 460 J/kg-°K (0–100°C)

Modulus of Elasticity 28.5 x 10<sup>6</sup> psi 196.5 GPa

Melting Range 2475-2525°F

2475-2525°F 1357-1385°C 460 J/kg-°K (0–100°C) Thermal Conductivity 212°F (100°C)

10.6 BTU/hr/ft²/ft/°F 18.3 W/m-°K

Electrical Resistivity 59.5 Microhm-in at 68°F 99 Microhm-cm at 20°C



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### Mean Coefficient of Thermal Expansion

Temperatu	re Range				
°F	°C	in/in°F	cm/cm°C		
200	93	7.9 x 10 <sup>-6</sup>	14.4 x 10 <sup>-6</sup>		
400	204	8.8 x 10 <sup>-6</sup>	15.9 x 10 <sup>-6</sup>		
600	316	9.0 x 10 <sup>-6</sup>	16.2 x 10 <sup>-6</sup>		
800	427	9.2 x 10 <sup>-6</sup>	16.5 x 10 <sup>-6</sup>		
1000	538	9.4 x 10 <sup>-6</sup>	16.8 x 10 <sup>-6</sup>		
1200	649	9.6 x 10 <sup>-6</sup>	17.1 x 10 <sup>-6</sup>		
1400	760	9.9 x 10 <sup>-6</sup>	17.5 x 10 <sup>-6</sup>		
1600	871	10.2 x 10⁻ <sup>6</sup>	18.0 x 10 <sup>-6</sup>		

# **Mechanical Properties**

Typical Values at 70°F (21°C)

Yield Strength 0.2% Offset		Ultimate Tensile Strength		Elongation in 2 in.	Hardness	
psi	(MPa)	psi	(MPa)	%		
29,000	200	77,000	531	52	126 Brinell	



High-temperature strength tensile properties of Alloys 800H and 800HT

## **Creep and Rupture Properties**

The tight chemistry control and solution annealing heat treatment were designed to provide optimum creep and rupture properties for Alloys 800H and 800HT. The following charts detail the outstanding creep and rupture properties of these alloys.



# Results of cyclic oxidation tests at 2000°F (1095°C). Cycles consisted of 15 min. heating and 5 min. cooling in air.



### **Representative Rupture-Strength Values for Alloys 800H/800HT**

Temperature		10,0	10,000 h		30,000 h		50,000 h		100,000 h	
°F	°C	ksi	MPa	ksi	MPa	ksi	MPa	ksi	MPa	
1200	650	17.5	121	15.0	103	14.0	97	13.0	90	
1300	705	11.0	76	9.5	66	8.8	61	8.0	55	
1400	760	7.3	50	6.3	43	5.8	40	5.3	37	
1500	815	5.2	36	4.4	30	4.1	28	3.7	26	
1600	870	3.5	24	3.0	21	2.8	19	2.5	17	
1700	925	1.9	13	1.6	11	1.4	10	1.2	8.3	
1800	980	1.2	8.3	1.0	6.9	0.9	6.2	0.8	5.5	

### **Oxidation Resistance**

The combination of the high nickel and chromium content in alloys 800H and 800HT provides excellent oxidation resistance properties to both alloys. The results of cyclic oxidation tests at both 1800°F (980°C) and 2000°F (1095°C) are shown below.





### **Corrosion Resistance**

The high nickel and chromium content of Alloys 800H and 800HT generally means they will have very similar aqueous corrosion resistance. The alloys have corrosion resistance that is comparable to 304 when used in nitric and organic acid service. The alloys should not be used in sulfuric acid service. They are subject to chromium carbide precipitation if in service for prolonged exposure in the 1000–1400°F (538–760°C) temperature range.

Since Alloys 800H and 800AT were developed primarily for hightemperature strength, corrosive environments to which these grades are exposed normally involve high temperature reactions such as oxidation and carburization.

### **Fabrication Data**

Alloys 800H and 800HT can be easily welded and processed by standard shop fabrication practices. However, because of the high strength of the alloys, they require higher powered process equipment than standard austenitic stainless steels.

### Hot Forming

The hot-working temperature range for Alloy 800H and 800HT is  $1740-2190^{\circ}F$  (950-1200°C) if deformation is 5 percent or greater. If the degree of hot deformation is less than 5 percent a hot working temperature range between  $1560-1920^{\circ}F$  ( $850-1050^{\circ}C$ ) is recommended. If the hot working metal temperature falls below the minimum working temperature, the piece must be re-heated. The alloys should be water quenched or rapid air cooled through the temperature range of  $1000-1400^{\circ}F$  ( $540-760^{\circ}C$ ). Alloys 800H and 800HT require solution annealing after hot working to ensure optimal creep resistance and properties.

#### **Cold Forming**

The alloys should be in the annealed condition prior to cold forming. Work hardening rates are higher than the austenitic stainless steels. This should be taken into account when selecting process equipment. An intermediate heat treatment may be necessary with a high degree of cold working or with more than 10 percent deformation.

### Welding

Alloys 800H and 800AT can be readily welded by most standard processes including GTAW (TIG), PLASMA, GMAW (MIG/MAG), and SMAW (MMA). The material should be in the solution-annealed condition, and free from grease, markings or scale. A post weld heat treatment is not necessary. Brushing with a stainless steel wire brush after welding will remove the heat tint and produce a surface area that does not require additional pickling.

### Machining

Alloys 800H and 800AT should preferably be machined in the annealed condition. Since the alloys are prone to work–hardening, only low cutting speeds should be used and the cutting tool should be engaged at all times. Adequate cut depth is necessary to assure avoiding contact with the previously formed work-hardened zone.

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